

# Effect of PWR Operational History on the Uncertainty of UNF's Radionuclide Inventory

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Holger Tietze-Jaensch, Ivan Fast and Yuliya Aksytina

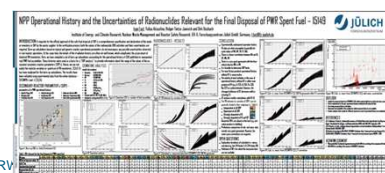
IEK-6 Institute for Energy and Climate Research,  
Nuclear Waste Management and Reactor Safety  
Research Center Jülich, Germany

PKS Product Quality Control Office for Radioactive Waste

## Outline

1. Disposability of Radioactive Waste in Germany
2. Nuclide Characterization, Inventory Declaration, Numerical Tools
3. Direct Disposal and PQC of Spent Fuel
4. Fuel Operational History & SRP Analysis of BU & CT
  - Parameter of an operational history of PWR
  - Determination of the limits and dependencies between SRPs
  - Downtime analysis
  - Results of burn-up calculations and comparison with experimental data from SFCOMPO database
5. Summary & Outlook

Poster at WMS 2015:

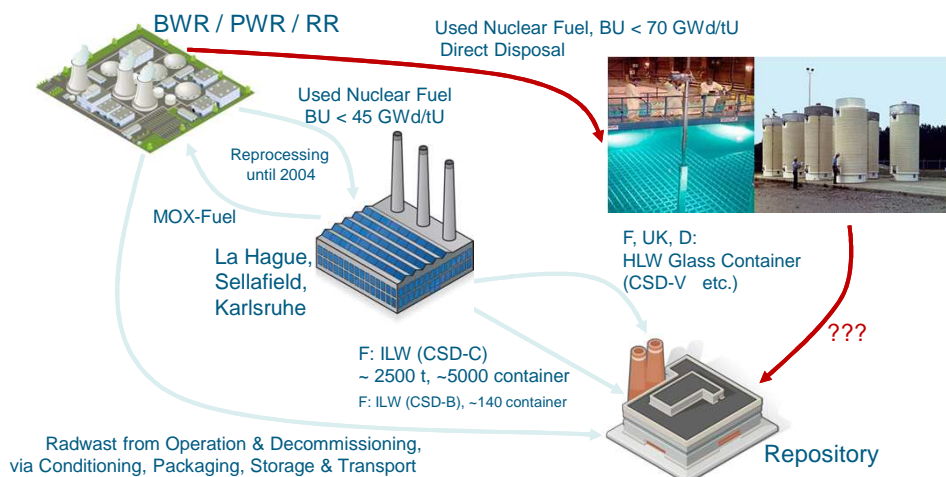


PQC: product quality control,  
SRP: secondary reactor parameters,  
BU: burn-up, CT: cooling time

## Nuclear Waste: What to Do After Use?



## German Radwaste: Waste Types, Origin & Streams



## Sources of Radioactive Waste

### 1. Operations

1. HLW: spent fuel element
  1. Reprocessing
  2. Direct disposal
  
2. LLW / ILW: solid & liquid operational waste
  1. Rinsing & filter residues
  2. Activated or contaminated waste

### 2. Decommissioning

1. HLW: spent fuel (cf. 1.1)
2. Solid / liquid waste (large quantities)

#### Professional

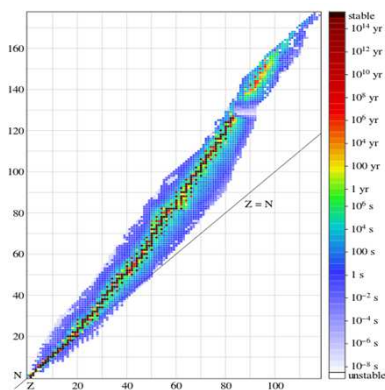
- Pre-Characterization
- Sorting
- Conditioning
- Full-Characterization
- Packing/ Containers
- Documentation
- Transport
- Interim Storage
- Final Disposal



Product Quality Control

## German HLW Repository Requirements

**KONRAD (LLW / ILW) Repository (under construction):**  
Positive permissible nuclide and materials list, i.e. nothing else is permitted for disposal !




Permissible radio-nuclides:

- Defined & fixed list of ~230 declarable & limited RN-activities for whole repository & every approved container.
- Max. permissible masses of toxic material for the whole repository and for each container.
- Max. activity & toxic levels are limited also from safety (MCA) assessment: incidents / accidents that may affect host rock, heat load, criticality survey



## Determination of a Standard Container Nuclear Inventory

Nucl. measurement	Measured nuclides	Calculated nuclides (families)
 <p>Photo: AREVA-NC, La Hague</p>	<b>Co-60</b>	<b>H-3</b> , Kr-85, I-129, C-14
	<b>Cs-134 Cs-137</b>	Cl-36, Ca-41, Mn-54, Fe-55, Co-58, Ni-59, Ni-63, Mo-93
	<b>Sb-125</b>	Ag-108m Ag-110m Cs-135
	<b>Eu-154</b>	Se-79, Sb-124, Sn-126
		(Ce+Pr)-144, Pm-147, Sm-151, Eu-152, Eu-155
		<b>(Sr+Y)-90</b> , Zr-93, Zr-95, Nb-94, Nb-95, Tc-99
		Ru-103, <b>(Rh+Ru)-106</b> , Pd-107
	Ra-226, Pa-231, Np-237, Am-241, Am-242m, Am-243, Cm-242, Cm-243, Cm-245, Cm-246, Cm-247, Cm-248, Cf-249, Cf-251, Cf-252	
	Th-229, Th-230, Th-232, U-232, U-233, U-234, U-236	
	Ac-227, Pu-238, Pu-240, Pu-242, Pu-243, Pu-244	

## Motivation

### Objectives

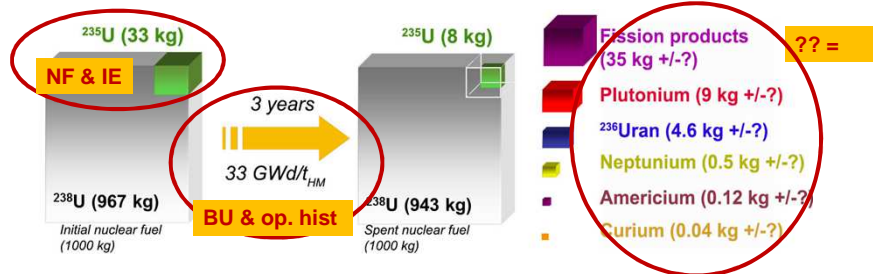
Knowledge of the composition of the radiological inventory of the radioactive waste

- for independent verification of the declared radwaste inventory by Product Quality Control
- for final disposal
- for long-term safety assessment

### Challenges

- The radwaste may contain different fuel assemblies (FA) with several operational histories (e.g. reprocessing products)
- Comprehensive information about the operational history may not be fully available

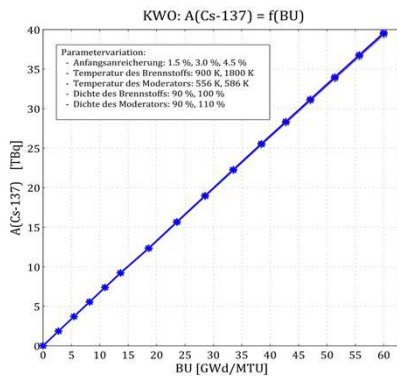
## Nuclear Inventory after Burn-Up: Operational History & SRP



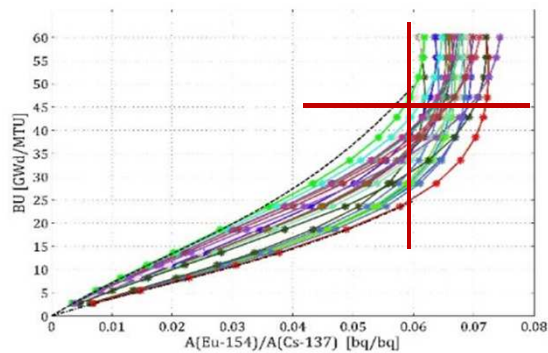
- SRP
- Operational history of burn-up (BU)
    - Specific power (SP), downtime (DT), irradiation time (IT)
  - Fuel properties
    - Initial enrichment (IE), density (FD), temperature (FT)
  - Moderator properties
    - Density (MD), temperature (MT), boric acid concentration (BA)

## Reactor Parameters (Fuel/Moderator) Influence BU Correlations

Cs-137 activity ~ burn-up (BU)  
(direct FP, i.e. no secondary reactor parameter dependence)



Eu-154/Cs-134 correlation ~ burn-up (BU)  
is not valid for high-BU > 45 GWd/t<sub>HM</sub>



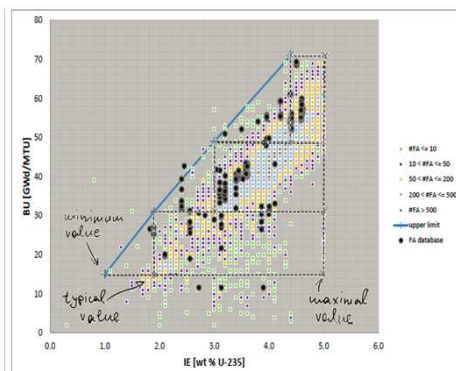
From I. Fast et al., WM2013

## Determination of the Limits and Dependencies Between the Secondary Reactor Parameters (SRP)

### Objectives

- Analysis of the whole spectrum of the secondary reactor parameters
- Using of the existing data of real spent fuel
- Using of existing theoretical models (if available)
- Building a fuel assembly (FA) database including comprehensive SRP data
- Determining the nuclide vectors of SNF with representative mean values and corresponding minimum and maximum bandwidths
- Validation of the simulation results with experimental data
- Determining the uncertainties of PWR radionuclide inventory by calculated and experimental data

## Downtime & SRP Analysis (BU vs. IE)



Ref.: J.M. Scaglione et. al., „Burnup Credit Approach Used in the Yucca Mountain License Application”, ORNL, 2010

### Overview on fuel assembly (FA)

- FA database contains 339 FA
  - 69 FA supplied from literature studies
  - 270 FA from industry submission
- The FA data base comprises information of the SRP mean values for whole irradiation period and often also details of the SRP-values and the associated reactor operating cycle

SRP: secondary reactor parameters,  
FA: fuel assembly



## Results of BU-Calculations (SCALE 6.1) and Comparison with Experimental Data (SFCOMPO)

### Nuclides to be declared for disposal in Germany:

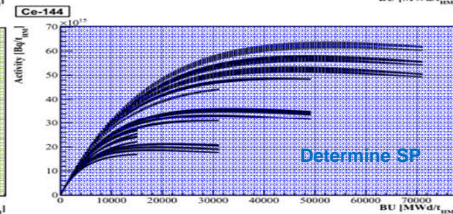
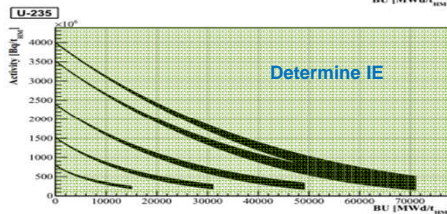
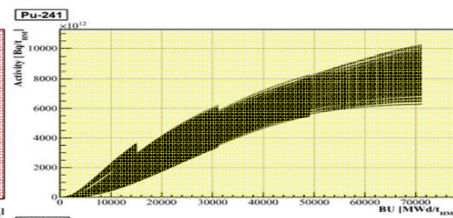
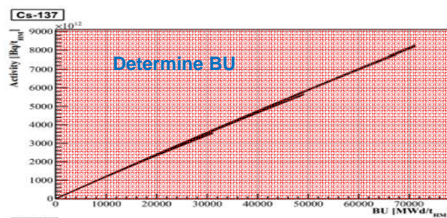
Ac-227, Ag-108m, Ag-110m, **Am-241**, **Am-242m**, **Am-243**, C-14, **Ce-144**, Cf-249, Cf-251, **Cm-242**, Cm-243, **Cm-244**, **Cm-245**, **Cm-246**, **Cm-247**, Cm-248, **Cs-134**, **Cs-135**, **Cs-137**, Eu-152, **Eu-154**, Eu-155, H-3, I-129, Kr-85, Mo-93, Nb-94, Nb-95, **Np-237**, Pa-231, Pd-107, Pm-147, Pr-144, **Pu-238**, **Pu-239**, **Pu-240**, **Pu-241**, **Pu-242**, Pu-243, Pu-244, Ra-226, Rh-106, Ru-103, **Ru-106**, Sb-124, **Sb-125**, **Se-79**, **Sm-151**, **Sn-126**, **Sr-90**, **Tc-99**, Th-229, Th-230, Th-232, **U-232**, U-233, **U-234**, **U-235**, U-236, **U-238**, Y-90, Zr-93, Zr-95

(in bold: SFCOMPO provides experimental data for comparison)

## BU-Calculation Results 1 (CT=0 & DT=0, IE = 1.0; 1.9; 3.0; 4.4; 5.0)

Varying SRP → 4 groups of RN behaviour:

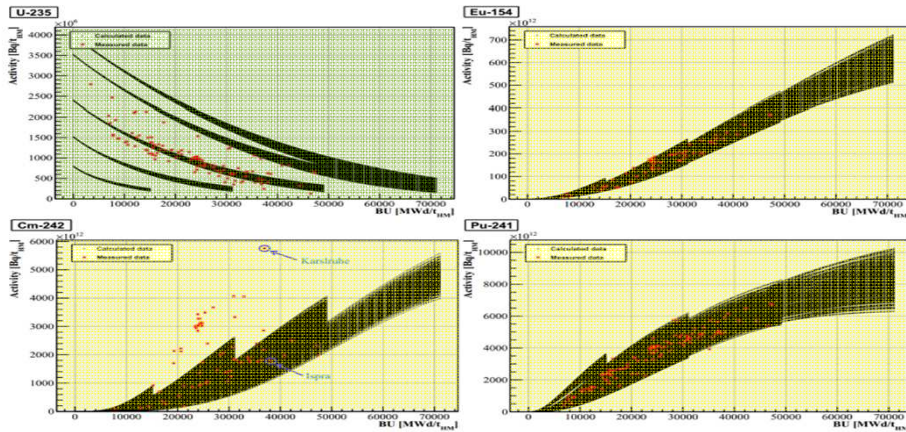
1. RN merely independent of all SRP
2. RN dependent of all SRP
3. RN strongly dependent of IE
4. RN strongly dependent of IE & SP



## BU-Calculation Results 2 (CT=0 & DT=0, IE = 1.0; 1.9; 3.0; 4.4; 5.0)

Exp. data (SFCOMPO) vs. numerical SRP variation:

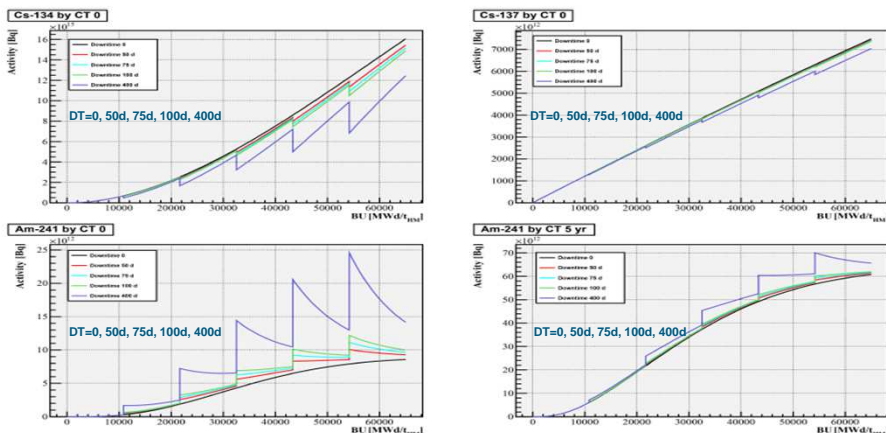
1. RN strongly dependent of IE
2. RN dependent of all SRP



15 Effect of Op-History & SRP on UNF Inventory H.Tietze-Jaensch et al., RWM Summer School #7, Ispra, Sep 2015

## Downtime Analysis & Theoretical Bandwidth of RN Activities:

1. RN activity conservative to DT=0
2. RN activity merely independent of DT
3. RN activity progressive to DT=0
4. RN activity mitigating for CT>>0



16 Effect of Op-History & SRP on UNF Inventory H.Tietze-Jaensch et al., RWM Summer School #7, Ispra, Sep 2015



## Downtime Analysis, Model Description

- Geometry: FA 16×16 AFA 3G (Siemens)
- Burn-up: 65 GWd/tHM
- Specific power: 36 MW/tHM
- Initial Enrichment: 4.0 % wt U-235
- Fuel temperature: 900 K
- Moderator temperature: 580 K
- Fuel density: 10.408 g/cm<sup>3</sup>
- Moderator density: 0.73 g/cm<sup>3</sup>
- Boric acid concentration: 460 ppm
- 6 Cycles with DT: 0, 50, 75, 100 and 400 days
- Analysis for cooling time (CT): 0, 1, 3 and 5 years

## Conclusion Table

(cf. I. Fast et al., Animma 2015, Lisbon, April 2015)

RN name <sup>1</sup>	$\delta_{CT}$ <sup>2</sup>	$\delta_{DT}$ <sup>3</sup>	# meas. data [3] <sup>4</sup>	Goodness [%] <sup>5</sup>									
Ac-227	+	(Z, Pa-231)	+	(DT, CT)	0	n.a.	Kr-85	-	(Z)	-	(DT)	0	n.a.
Ag-108m	0		0	0	n.a.	Mo-93	0		+	(DT)	0	n.a.	
Ag-110m	-	(Z)	-	(DT)	0	Nb-94	0		-	(DT)	0	n.a.	
Am-241	+	(Z, Pu-241)	+	(DT, CT)	68	Np-237	0		-	(DT, CT)	0	n.a.	
Am-242m	0		+	(DT)	24	Pd-107	0		+	(DT, BU, CT)	0	n.a.	
Am-243	0		0	47	100	Pm-147	-	(Z)	-	(DT)	0	n.a.	
C-14	0		0	0	n.a.	Po-144	-	(Z)	-	(DT)	0	n.a.	
Ce-144	-	(Z, Pu-241)	-	(DT)	16	Pu-238	0		-	(DT)	90	87	
Cf-249	0		0	0	n.a.	Pu-239	0				115	96	
Cf-251	0		0	0	n.a.	Pu-240	0				113	100	
Cm-242	-	(Z, Am-242m)	+	(DT)	71	Pu-241	-	(Z, Cm-245)	0		113	100	
Cm-243	-	(Z)	+	(DT)	0	Pu-242	0				90	99	
Cm-244	-	(Z)	0	76	100	Pu-243	0				0	n.a.	
Cm-245	0		0	11	100	Pu-244	0				0	n.a.	
Cm-246	0		0	11	100	Ra-226	+	(Z, Th-230)	+	(DT, CT)	0	n.a.	
Cm-247	0		0	5	100	Rb-106	-	(Z)	-	(DT)	0	n.a.	
Cm-248	0		0	0	n.a.	Ru-103	-	(Z)	0	0	n.a.		
Cs-134	-	(Z)	-	(DT)	56	Ru-106	-	(Z)	-	(DT)	27	96	
Cs-135	0		-	(DT)	9	Sb-124	-	(Z)	0	0	n.a.		
Cs-137	-	(Z)	-	(DT)	69	Sb-125	-	(Z)	-	(DT)	27	44	
Eu-152	-	(Z)	+	(DT, BU)	0	Se-79	0		0	8	0		
Eu-154	-	(Z)	0	56	100	Sm-151	0		-	(DT)	6	100	
Eu-155	-	(Z)	0	0	n.a.	Sn-126	0		0	9	0		
H-3	-	(Z)	0	0	n.a.	Sr-90	-	(Z)	-	(DT)	10	80	
I-129	0		0	0	n.a.	Tc-99	0		+	(DT)	0	13	
						Th-229	0		+	(DT)	0	n.a.	
						Th-230	+	(Z, U-234)	+	(DT, CT)	0	n.a.	
						Th-232	+	(Z, U-236)	+	(DT, CT)	0	n.a.	
						U-232	+	(Z)	+	(DT, CT)	10	0	
						U-233	+	(Z, Np-237)	+	(DT, CT)	0	n.a.	
						U-234	+	(Z, Pu-238)	+	(DT, CT)	30	0	
						U-235	0		0	115	100		
						U-236	0		0	0	n.a.		
						U-238	0		0	90	88		
						Y-90	-	(Z)	-	(DT)	0	n.a.	
						Zr-93	0		0	0	n.a.		
						Zr-95	-	(Z)	-	(DT)	0	n.a.	

## Explanations of Previous Table

1. The color describes the RN behavior to the variation of SRPs. There are four groups: RN independent of all SRP red, RN dependent of all SRP yellow, RN strongly dependent of IE green and RN strongly dependent of IE and SP blue.
2. CT is the correction factor of post-irradiation cooling time for measured data. This factor is a function of the own decay (Z) rate of that RN and applicable on the parent RN. The sign denotes positive or negative impact on the RN activity relatively to CT=0. The size of the sign shows the magnitude of this influence.
3. DT is the correction factor of down time for the theoretical bandwidth. The sign denotes positive or negative impact on the RN activity relatively to the theoretical bandwidth for DT=0. Again, the size of the sign shows the magnitude of this influence.
4. The number of individual radiochemical measurements of several samples from the SFCOMPO-1 database. Goodness provides the quality of agreement (in %) of calculated vs. measured data, i.e. number of measured data within the theoretical bandwidth; n.a.: not applicable.

## Summary

### Summary

- Comparison of calculated and measured data reveals good agreement. However, for some cases correction is required.
- Missing measured data for high burn-up
- The nuclides are differently influenced by a variation of the operational history, revealing different behavior:
  - Independent of all SRP: Se-79, Tc-99, Cs-137
  - Dependence of all SRP: C-14, Am-241, Am-242, Pu-239, Pu-241 etc.
  - Strong dependence of IE: Zr-93, I-129, Eu-155, U-235, Am-243m, etc.
  - Strong dependence of IE & SP: Nb-95, Zr-95, Ru-106, Sb-126, Ce-144, Ac-227, etc.

## Conclusion

1. Experimentally underpinned operation history FA data are often incomplete (especially for cycle averaged values of MD, MT, FD, FT, BA).
2. It is feasible to determine the SRP variability limits.
3. We have performed burn-up calculations for 64 RN relevant for the final disposal of radioactive waste. Activation products were not considered.
4. For most fission products the calculations assuming an operational history with DT=0 are either independent of DT or overestimated (exceptions: Eu-152, Mo-93).
5. Many actinides activities (operational history with DT=0) are either independent of DT (e.g. U-235, U-238, Pu-239, Np-237) or underestimated (e.g. Ac-227, Am-241, Cm-242, Ra-226).
6. DT analysis enables calculations with DT=0. In the case of activities systematically over- or underestimated, resp., the theoretical bandwidths must be corrected <sup>IF17</sup>
7. Due to the variation of the SRP values the RN behavior can be generally divided into 4 groups.
8. Comparison of calculated and measured data reveals generally good agreement. However, for some RNs a comprehensive agreement between calculated and measured values requires corrections as specified in the table above.
9. The uncertainty of the radionuclide inventory of PWR spent fuel computed on the basis of real operational history data is less than one order of a magnitude of the actual activity of the relevant radionuclide.

## Appendix: Numerical Methodology



## Slide 21

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**IF17** corrected  
Ivan Fast, 8/23/2015

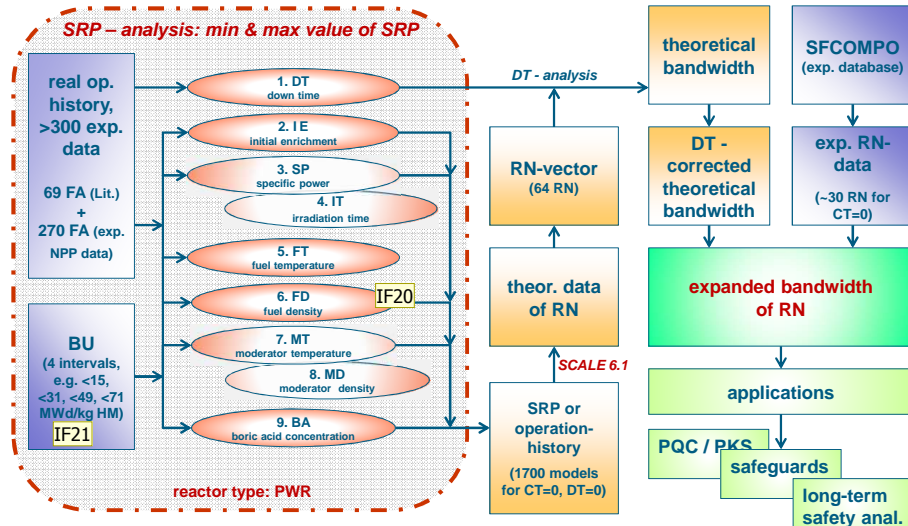
## Slide 22

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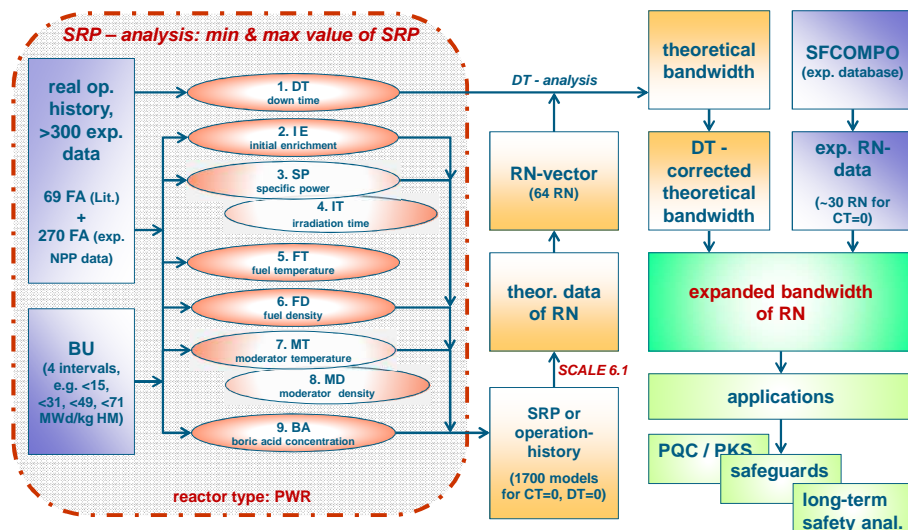
**IF18** Ich würde hier einfach "Theoretical bandwidth ..." schreiben. Hier braucht man noch keine detaillierte Beschreibung.  
Ivan Fast, 8/23/2015

**IF19** Ich würde hier einfach "Expanded bandwidth of radionuclides" schreiben. es ist auch klar, das es die selbe Radionuklide gemeint wie bei theoretischer Bandbreite  
Ivan Fast, 8/23/2015

## Appendix: Numerical Methodology



## Appendix: Numerical Methodology



## Slide 23

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**IF20** Fuel density würde ich auch klein schreiben wie alle andere SRP oder alle groß.

Ivan Fast, 8/23/2015

**IF21** Hier würde ich in Klammern entweder nur "4 intervals" schreiben oder Intervalle richtig schreiben "0-15, 0-31, 0-49 und 0-71"

Ivan Fast, 8/23/2015



## Applications

### Applications

- PQC: product quality control of FA packages for direct disposal
- Nuclear forensic / safeguards
- Long-term safety assessment of UNF / SNF behaviour
- ...

## Acknowledgement to:

1. Wissenschaftlich Technische Ingenieurberatung GmbH (WTI), Jülich for FA data
2. NEA for SFCOMPO (2) access

## Thank You for Your Attention!



Of course we can do  
a lot better than this



We must decide on the way forward  
and not linger